

**DYNAMIC DECOMPOSITION OF APPARENT POWER IN  
POLYPHASE UNBALANCED NETWORKS WITH APPLICATION  
TO TRANSIENTS IN AN INDUSTRIAL LOAD**

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## PREVIEW AND MOTIVATION

- Our (earlier) static 7-component decomposition of apparent power refines several known results, including Czarnecki's 5-component decomposition (CPC).
- We rely on the concept of dynamic phasors to make our decomposition **dynamic**, allowing it to capture transient behavior.
- Two of our 7 components – the real power  $P$  and Budeanu's reactive power  $Q_B$  – are network conservative. We split these two into their symmetric sequence components (all conservative as well), which results in a new two-level, 7/11-component decomposition of apparent power.

## OVERVIEW

- Hilbert Space of Periodic Polyphase Waveforms
- Orthogonal Current Decomposition
- 7-Component Power Decomposition
- Network-Conservative Power Components
- 7/11-Component Power Decomposition
- Local Hilbert Space and Dynamic Phasors
- Industrial Example
- Concluding Remarks

## HILBERT SPACE FRAMEWORK

Space elements: real-valued  $T$ -periodic square-integrable polyphase waveforms

$$x(t) = \begin{bmatrix} x_1(t) & x_2(t) & \dots & x_n(t) \end{bmatrix} \quad (\text{row vector})$$

Inner product and norm:

$$\langle x, y \rangle \stackrel{\text{def}}{=} \frac{1}{T} \int_T x(t) y(t)^\top dt \quad \|x\| \stackrel{\text{def}}{=} \sqrt{\langle x, x \rangle}$$

Fourier coefficients:

$$X_\ell \stackrel{\text{def}}{=} \frac{1}{T} \int_T x(t) e^{-j\ell\omega t} dt$$

$X_{k,\ell}$  is the  $k$ -th element of the phasor vector  $X_\ell$ .

Parseval identity:

$$\langle x, y \rangle = \sum_{\ell=-\infty}^{\infty} X_\ell Y_\ell^H = \sum_{k=1}^n \sum_{\ell=-\infty}^{\infty} X_{k,\ell} Y_{k,\ell}^*$$

## STATIC ORTHOGONAL CURRENT DECOMPOSITION

$$i(t) = \underbrace{\sum_{k,l} g_{k,l} v_{k,l}(t)}_{i_v(t)} \oplus \underbrace{\sum_{k,l} b_{k,l} \mathcal{H}v_{k,l}(t)}_{i_w(t)} \oplus i_{\perp}(t)$$

where

$$g_{k,l} \stackrel{\text{def}}{=} \frac{\langle i, v_{k,l} \rangle}{\|v_{k,l}\|^2}, \quad b_{k,l} \stackrel{\text{def}}{=} \frac{\langle i, \mathcal{H}v_{k,l} \rangle}{\|v_{k,l}\|^2}$$

Equivalent linear load:

$$i_{k,l}(t) = g_{k,l} v_{k,l}(t) + b_{k,l} \mathcal{H}v_{k,l}(t) = 2 \Re \left\{ \underbrace{(g_{k,l} - j b_{k,l}) V_{k,l}}_{I_{k,l}} e^{j\ell\omega t} \right\} \underbrace{[0 \dots 0 \mathbf{1} 0 \dots 0]}_k$$

⇓

$$(k, \ell)\text{-admittance} \stackrel{\text{def}}{=} \frac{I_{k,l}}{V_{k,l}} = g_{k,l} - j b_{k,l}$$

The Hilbert transform:

$$\mathcal{H} \{ e^{j\ell\omega t} \} \stackrel{\text{def}}{=} -j \operatorname{sgn}(\ell) e^{j\ell\omega t}$$

## 5-COMPONENT DECOMPOSITION

Conductance spread (average, variance):  $i_v(t) = i_F(t) \oplus i_g(t)$

$i_F(t) \iff \mu_g$ , weighted mean of  $g_{k,\ell}$

$i_g(t) \iff$  spread of  $g_{k,\ell}$  around  $\mu_g$

Susceptance spread (average, variance):  $i_w(t) = i_B(t) \oplus i_b(t)$

$i_B(t) \iff \mu_b$ , weighted mean of  $b_{k,\ell}$

$i_b(t) \iff$  spread of  $b_{k,\ell}$  around  $\mu_b$

## 5-COMPONENT DECOMPOSITION (continued)

### 5-component decomposition:

$$i(t) = \underbrace{i_F(t) \oplus i_g(t)}_{i_v(t)} \oplus \underbrace{i_B(t) \oplus i_b(t)}_{i_w(t)} \oplus i_{\perp}(t)$$

$$S^2 = (P^2 + N_g^2) + (Q_B^2 + Q_b^2) + S_{\perp}^2$$

$$S \stackrel{\text{def}}{=} \|i\| \|v\| , \quad N_g \stackrel{\text{def}}{=} \|i_g\| \|v\| , \quad Q_b \stackrel{\text{def}}{=} \|i_b\| \|v\| , \quad S_{\perp} \stackrel{\text{def}}{=} \|i_{\perp}\| \|v\|$$

Shepherd & Zakikhani	$S_R$	$S_X$
Ours	$i_v, S_v$	$i_w, Q_w$

Sharon	$P$	$S_c$	$S_Q$
Ours	$i_F, P$	$i_g, N_g$	$i_w, Q_w$

$$S_v \stackrel{\text{def}}{=} \|i_v\| \|v\| = \sqrt{P^2 + N_g^2} , \quad Q_w \stackrel{\text{def}}{=} \|i_w\| \|v\| = \sqrt{Q_B^2 + Q_b^2}$$

## EFFECT OF UNBALANCED LOAD

Splitting of  $i_g$ :       $i_v(t) = i_F(t) \oplus \underbrace{i_{gs}(t) \oplus i_{gu}(t)}_{i_g(t)}$

$i_{gs}(t) \iff \mu_g(\ell)$ , weighted conditional mean of  $g_{k,\ell}$

$i_{gu}(t) \iff$  spread of  $g_{k,\ell}$  around  $\mu_g(\ell)$       (g-balanced load  $\Leftrightarrow i_{gu} = 0$ )

Splitting of  $i_b$ :       $i_w(t) = i_B(t) \oplus \underbrace{i_{bs}(t) \oplus i_{bu}(t)}_{i_b(t)}$

$i_{bs}(t) \iff \mu_b(\ell)$ , weighted conditional mean of  $b_{k,\ell}$

$i_{bu}(t) \iff$  spread of  $b_{k,\ell}$  around  $\mu_b(\ell)$       (b-balanced load  $\Leftrightarrow i_{bu} = 0$ )

## 7-COMPONENT DECOMPOSITION

$$i(t) = \underbrace{i_F(t) \oplus i_{gs}(t) \oplus i_{gu}(t)}_{i_w(t)} \oplus \underbrace{i_B(t) \oplus i_{bs}(t) \oplus i_{bu}(t)}_{i_w(t)} \oplus i_{\perp}(t)$$

$$S^2 = P^2 + \underbrace{N_s^2 + N_u^2}_{N_g^2} + Q_B^2 + \underbrace{Q_s^2 + Q_u^2}_{Q_b^2} + S_{\perp}^2$$

$$N_s \stackrel{\text{def}}{=} \|i_{gs}\| \|v\| , \quad N_u \stackrel{\text{def}}{=} \|i_{gu}\| \|v\| , \quad Q_s \stackrel{\text{def}}{=} \|i_{bs}\| \|v\| , \quad Q_u \stackrel{\text{def}}{=} \|i_{bu}\| \|v\|$$

Czarnecki	$i_a$	$i_s$	$i_r$	$i_u$	$i_g$
Ours	$i_F$	$i_{gs}$	$i_B \oplus i_{bs}$	$i_{gu} \oplus i_{bu}$	$i_{\perp}$

**Notice:** Budeanu's reactive power  $Q_B$  is a subcomponent of Czarnecki's  $Q_r$ .

## NETWORK-CONSERVATIVE POWER COMPONENTS

Telegen's theorem: implies that the quantity  $\langle \mathcal{A}i, \mathcal{B}v \rangle$  is *network-conservative* for any two linear operators  $\mathcal{A}$  and  $\mathcal{B}$  that are invariant across the network.

This means that

$$\sum_m \langle \mathcal{A}i_m, \mathcal{B}v_m \rangle = 0$$

in any closed system of interconnected (lumped) elements, where  $v_m(t)$  denotes the voltage across the  $m$ -th element, and  $i_m(t)$  is the current flowing into the same element.

Example: our two signed power components

$$P = \langle i, v \rangle = \mu_g \|v\|^2 = 2 \sum_{k,\ell} |I_{k,\ell}| |V_{k,\ell}| \cos(\arg(V_{k,\ell} I_{k,\ell}^*))$$

$$Q_B = \langle i, \mathcal{H}v \rangle = \mu_b \|v\|^2 = 2 \sum_{k,\ell} |I_{k,\ell}| |V_{k,\ell}| \sin(\arg(V_{k,\ell} I_{k,\ell}^*))$$

## 7/11-COMPONENT POWER DECOMPOSITION

Decompose signed power components:

$$P = \underbrace{\langle i_+, v \rangle}_{P_+} + \underbrace{\langle i_-, v \rangle}_{P_-} + \underbrace{\langle i_0, v \rangle}_{P_0}$$

$$Q_B = \underbrace{\langle i_+, \mathcal{H}v \rangle}_{Q_{B,+}} + \underbrace{\langle i_-, \mathcal{H}v \rangle}_{Q_{B,-}} + \underbrace{\langle i_0, \mathcal{H}v \rangle}_{Q_{B,0}}$$

$i_+(t)$ ,  $i_-(t)$ ,  $i_0(t)$  are the positive, negative, and zero-sequence components of  $i(t)$ .

All six subcomponents –  $P_+$ ;  $P_-$ ;  $P_0$ ;  $Q_{B,+}$ ;  $Q_{B,-}$ ;  $Q_{B,0}$  – are network-conservative.

Two-level power decomposition:

$$S^2 = (P_+ + P_- + P_0)^2 + (Q_{B,+} + Q_{B,-} + Q_{B,0})^2 + N_s^2 + N_u^2 + Q_s^2 + Q_u^2 + S_{\perp}^2$$

## LOCAL HILBERT SPACE AND DYNAMIC PHASORS

Space elements: real-valued polyphase waveforms that are square-integrable on the interval  $(t - T \quad t]$  for every  $t$ .

$$x(t) = \left[ x_1(t) \quad x_2(t) \quad \dots \quad x_n(t) \right] \quad (\text{row vector})$$

Inner product and norm:

$$\langle x, y \rangle(t) \stackrel{\text{def}}{=} \frac{1}{T} \int_{t-T}^T x(s) y(s)^\top ds \quad \| x \| (t) \stackrel{\text{def}}{=} \sqrt{\langle x, x \rangle(t)}$$

Dynamic phasors:

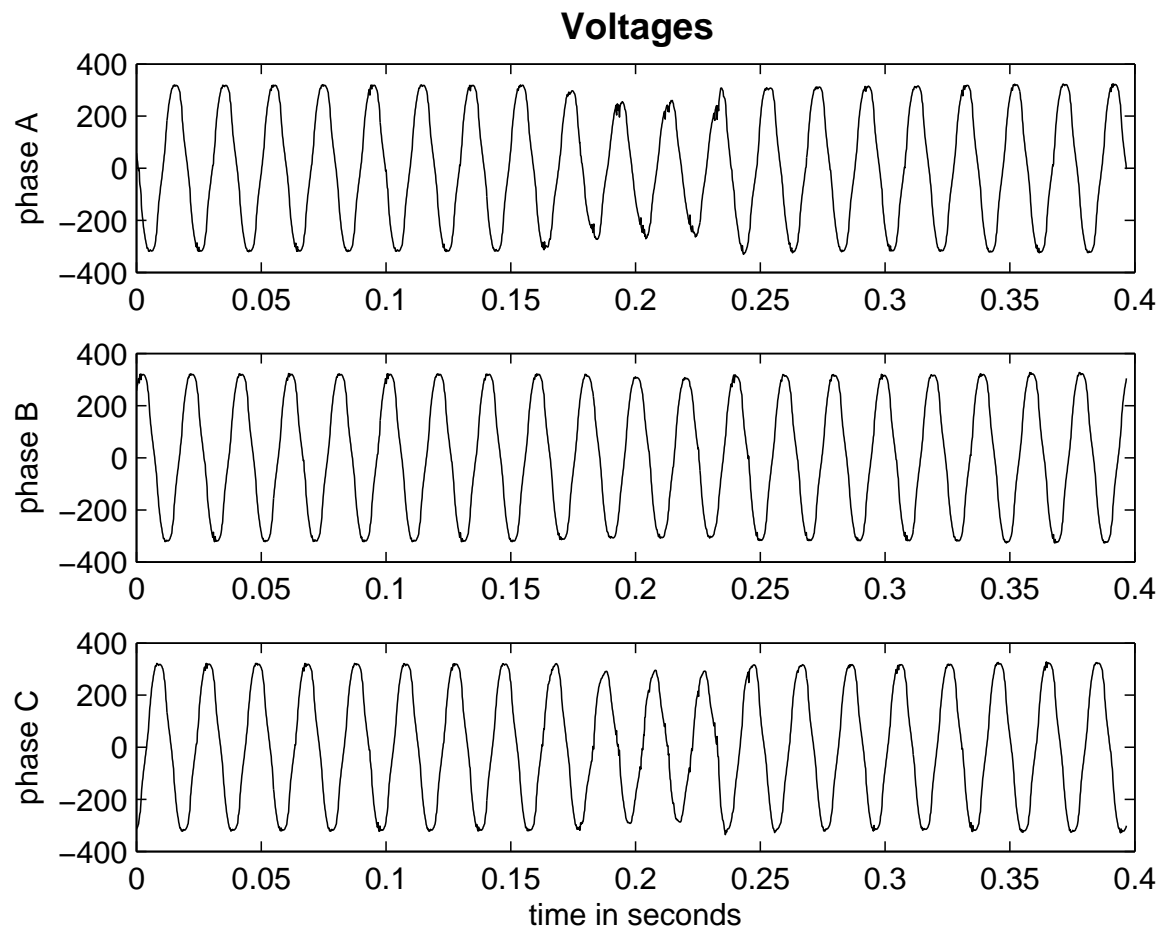
$$X_\ell(t) \stackrel{\text{def}}{=} \frac{1}{T} \int_{t-T}^T x(s) e^{-j\ell\omega s} ds$$

$X_{k,\ell}(t)$  is the  $k$ -th element of the phasor vector  $X_\ell(t)$ .

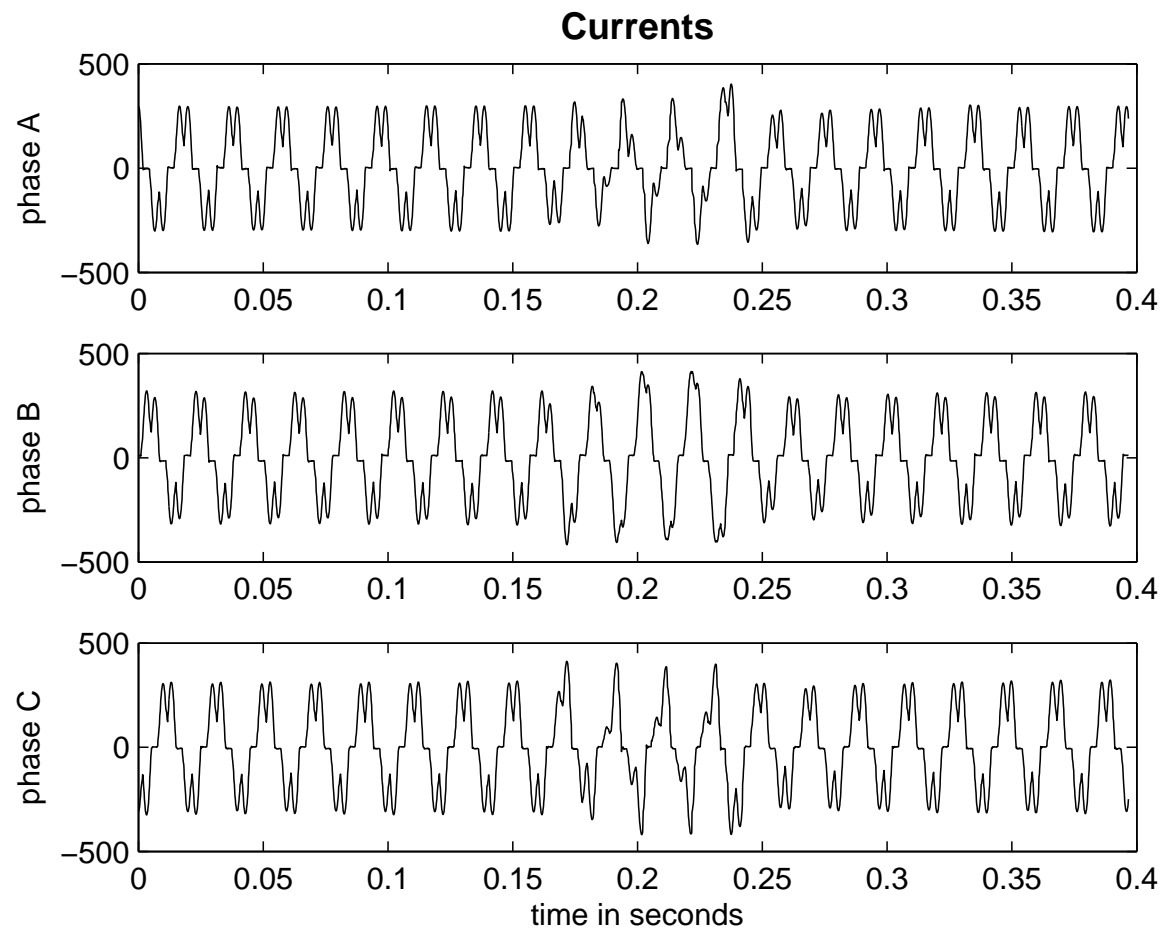
Parseval:

$$\langle x, y \rangle(t) = \sum_{\ell=-\infty}^{\infty} X_\ell(t) Y_\ell^H(t) = \sum_{k=1}^n \sum_{\ell=-\infty}^{\infty} X_{k,\ell}(t) Y_{k,\ell}^*(t)$$

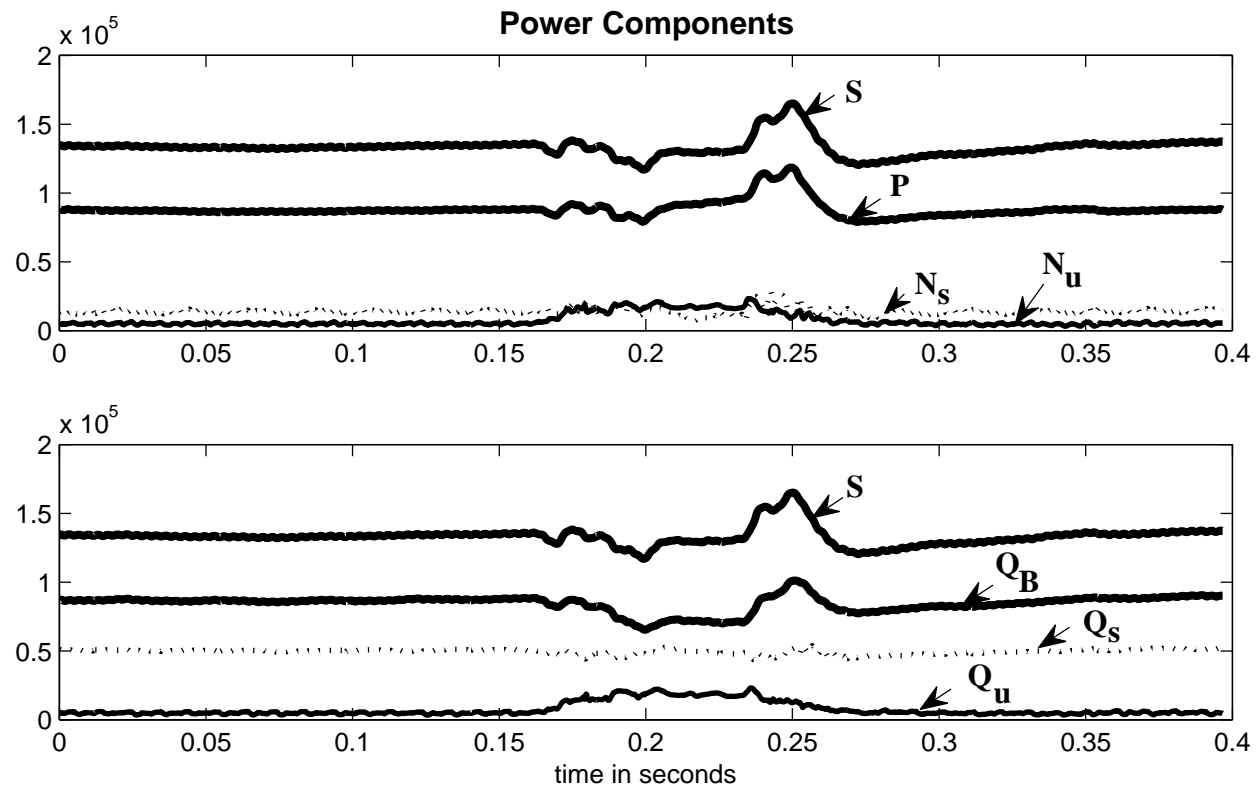
## INDUSTRIAL EXAMPLE – paper plant during an outage [14]



## INDUSTRIAL EXAMPLE – continued

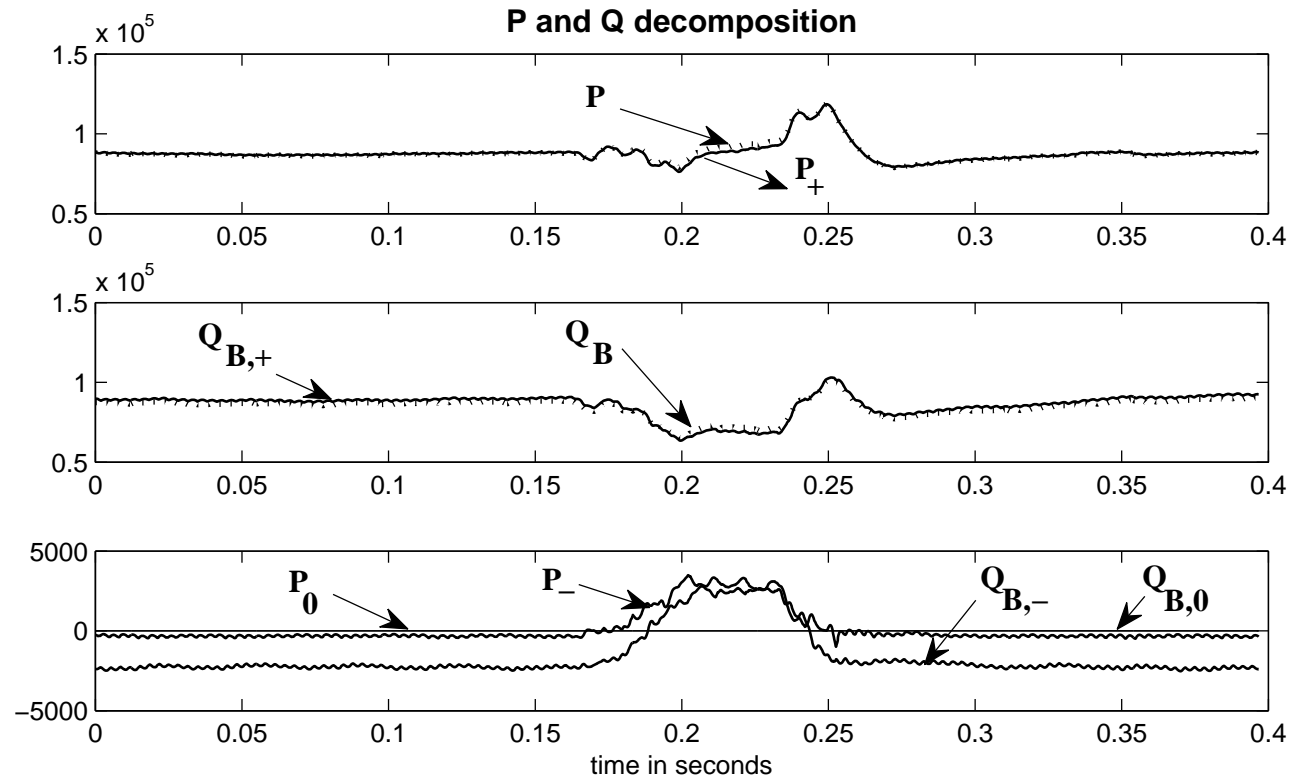


## INDUSTRIAL EXAMPLE – continued



**Notice:**  $N_u(t)$  and  $Q_u(t)$  have significant values only during the fault.

## INDUSTRIAL EXAMPLE – continued

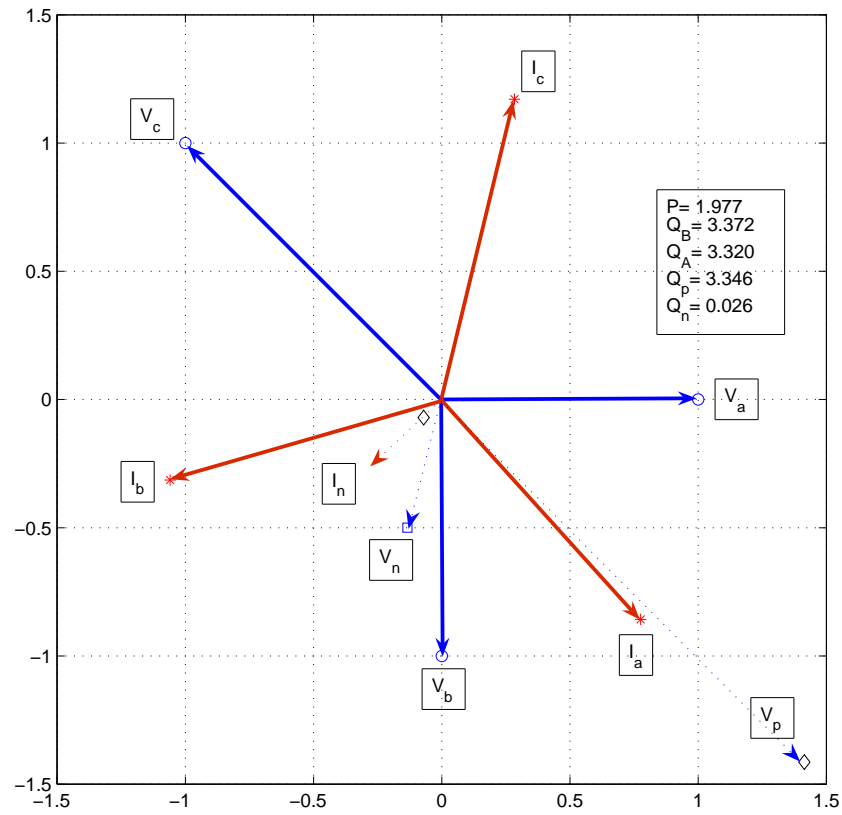


**Notice:**  $P_-(t)$  (and  $Q_{B,-}(t)$ ) exhibit significant transients during the fault.

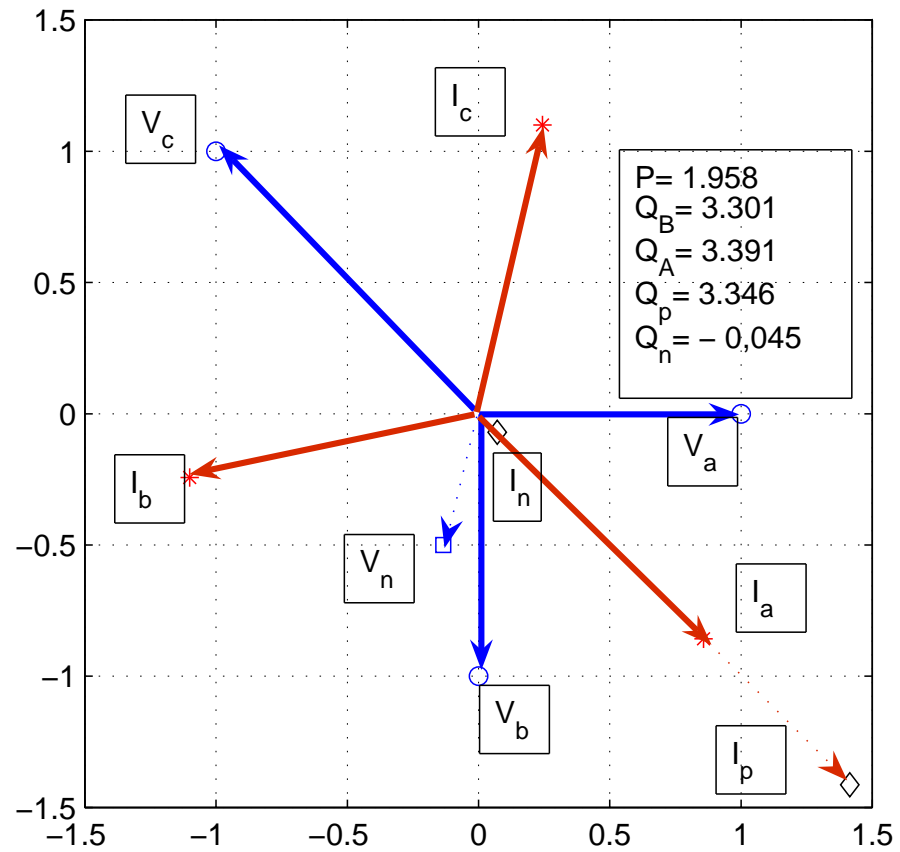
## CONCLUDING REMARKS

- Our 7-component decomposition is a refinement of Czarnecki, Sharon, Shepherd & Zakikhani, as well as Budeanu and Fryze. It serves to illuminate the relations between these classical decompositions.
- The refined, two-level, 7/11-component decomposition provides further detail – the sequence components of  $P$  and  $Q_B$  (all network-conservative).
- Relying on dynamic phasors makes our decompositions time-variant, allowing to capture transient behavior.
- The example demonstrates the intuitive appeal of our dynamic current/power decompositions.

## INDUSTRIAL EXAMPLE – continued



## INDUSTRIAL EXAMPLE – continued



## 5-COMPONENT DECOMPOSITION

Conductance spread (average, variance):

$$i_F(t) = \mu_g v(t) \quad , \quad \mu_g \stackrel{\text{def}}{=} \frac{P}{\|v\|^2} = \sum_{k,l} p_{k,l} g_{k,l} \quad , \quad p_{k,l} \stackrel{\text{def}}{=} \frac{\|v_{k,l}\|^2}{\|v\|^2}$$

$$i_v(t) = i_F(t) \oplus i_g(t) \quad , \quad i_g(t) = \sum_{k,l} (g_{k,l} - \mu_g) v_{k,l}(t)$$

$i_F(t) \iff$  weighted mean of  $g_{k,l}$

$i_g(t) \iff$  spread of  $g_{k,l}$  around  $\mu_g$

$$\|i_g\| = \sigma_g \|v\| \quad , \quad \sigma_g \stackrel{\text{def}}{=} \sqrt{\sum_{k,l} p_{k,l} (g_{k,l} - \mu_g)^2} \quad (g_{k,l} = \text{const.} \iff i_g = 0)$$

## 5-COMPONENT DECOMPOSITION (continued)

Susceptance spread (average, variance):

$$i_B(t) = \mu_b \mathcal{H}v(t) \quad , \quad \mu_b \stackrel{\text{def}}{=} \sum_{k,\ell} p_{k,\ell} b_{k,\ell}$$

$$i_w(t) = i_B(t) \oplus i_b(t) \quad , \quad i_b(t) = \sum_{k,\ell} (b_{k,\ell} - \mu_b) \mathcal{H}v_{k,\ell}(t)$$

$i_B(t) \iff$  weighted mean of  $b_{k,\ell}$

$i_b(t) \iff$  spread of  $b_{k,\ell}$  around  $\mu_b$

$$\|i_b\| = \sigma_b \|v\| \quad , \quad \sigma_b \stackrel{\text{def}}{=} \sqrt{\sum_{k,\ell} p_{k,\ell} (b_{k,\ell} - \mu_b)^2} \quad ( b_{k,\ell} = \text{const.} \iff i_b = 0 )$$

## EFFECT OF UNBALANCED LOAD – conductances

### Splitting of $i_g$ :

$$i_v(t) = i_F(t) \oplus \underbrace{i_{gs}(t) \oplus i_{gu}(t)}_{i_g(t)} \quad , \quad \mu_g(\ell) \stackrel{\text{def}}{=} \frac{\sum_k g_{k,\ell} p_{k,\ell}}{\sum_k p_{k,\ell}}$$

$$i_{gs}(t) = \sum_{k,\ell} [\mu_g(\ell) - \mu_g] v_{k,\ell}(t) \quad , \quad i_{gu}(t) = \sum_{k,\ell} [g_{k,\ell} - \mu_g(\ell)] v_{k,\ell}(t)$$

### Spread of $g_{k,\ell}$ :

$$\|i_{gu}\| = \sigma_{gu} \|v\| \quad , \quad \sigma_{gu} \stackrel{\text{def}}{=} \sqrt{\sum_{k,\ell} p_{k,\ell} |g_{k,\ell} - \mu_g(\ell)|^2} \quad (\text{g-balanced load} \Leftrightarrow i_{gu} = 0)$$

$$\|i_{gs}\| = \sigma_{gs} \|v\| \quad , \quad \sigma_{gs} \stackrel{\text{def}}{=} \sqrt{\sum_{k,\ell} p_{k,\ell} |\mu_g(\ell) - \mu_g|^2} \quad (\sigma_g^2 = \sigma_{gs}^2 + \sigma_{gu}^2)$$

## EFFECT OF UNBALANCED LOAD - susceptances

### Splitting of $i_b$ :

$$i_w(t) = i_B(t) \oplus \underbrace{i_{bs}(t) \oplus i_{bu}(t)}_{i_b(t)} \quad , \quad \mu_b(\ell) \stackrel{\text{def}}{=} \frac{\sum_k b_{k,\ell} p_{k,\ell}}{\sum_k p_{k,\ell}}$$

$$i_{bs}(t) = \sum_{k,\ell} [\mu_b(\ell) - \mu_b] \mathcal{H}v_{k,\ell}(t) \quad , \quad i_{bu}(t) = \sum_{k,\ell} [b_{k,\ell} - \mu_b(\ell)] \mathcal{H}v_{k,\ell}(t)$$

### Spread of $b_{k,\ell}$ :

$$\|i_{bu}\| = \sigma_{bu} \|v\| \quad , \quad \sigma_{bu} \stackrel{\text{def}}{=} \sqrt{\sum_{k,\ell} p_{k,\ell} |b_{k,\ell} - \mu_b(\ell)|^2} \quad (\text{b-balanced load} \Leftrightarrow i_{bu} = 0)$$

$$\|i_{bs}\| = \sigma_{bs} \|v\| \quad , \quad \sigma_{bs} \stackrel{\text{def}}{=} \sqrt{\sum_{k,\ell} p_{k,\ell} |\mu_b(\ell) - \mu_b|^2} \quad (\sigma_b^2 = \sigma_{bs}^2 + \sigma_{bu}^2)$$