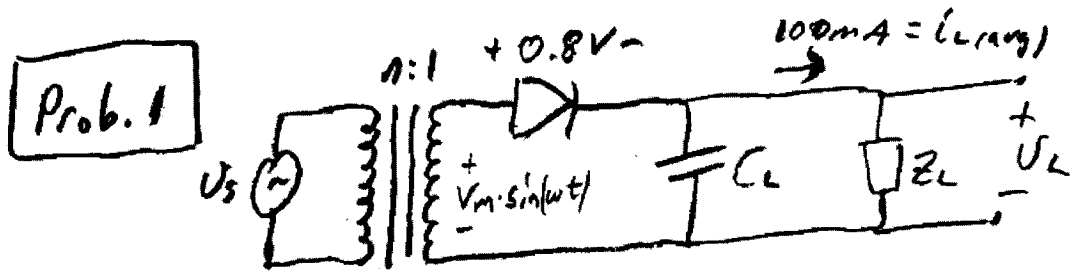


①

Homework 4 Solutions

Fall
2018

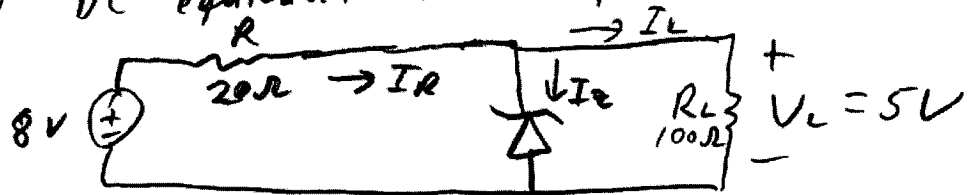


- 1.) $V_L(\text{avg}) = 9V \pm 1V$ ripple
(2V peak-peak) \rightarrow $V_L(\text{min}) = 8V$
- $V_L(\text{max}) = 10V$
- 2.) KVL:
 $V_L(\text{peak}) = -0.8V + V_m = 10V \rightarrow V_m = 10.8V$
- 3.) $V_s(\text{peak}) = V_s(\text{RMS}) \cdot \sqrt{2} = 110V \cdot \sqrt{2} = 155.563V$
- $n = \frac{V_s(\text{peak})}{V_m} = \frac{155.563V}{10.8V} = 14.4 = n$
- 4.) Using equation 3.4 in the book:
 $C = \frac{i_{L(\text{avg})} \cdot T}{V_r} = \frac{(100\text{mA}) \cdot (\frac{1}{60\text{Hz}})}{2V}$

②

Problem 2

DC equivalent circuit for Q-point analysis:



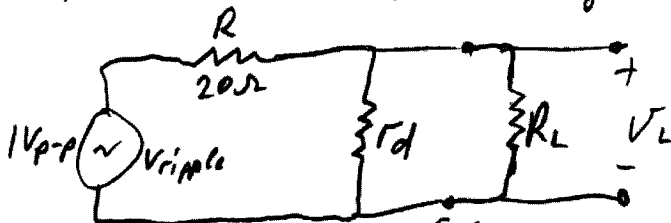
$$I_R = \frac{8V - 5V}{20\Omega} = 150mA$$

$$I_L = \frac{5V}{100\Omega} = 50mA$$

$$KCL: I_R = I_L + I_Z \rightarrow I_Z = 150mA - 50mA = 100mA$$

$$I_{ZQ-point} = 100mA$$

Equivalent circuit for AC analysis:



$$V_L = V_{ripple} \cdot \left(\frac{R_L \parallel r_d}{R_L \parallel r_d + R} \right)$$

$$V_L = V_{ripple} \cdot \frac{\left(\frac{1}{R_L} + \frac{1}{r_d} \right)^{-1}}{\left(\frac{1}{R_L} + \frac{1}{r_d} \right)^{-1} + R}$$

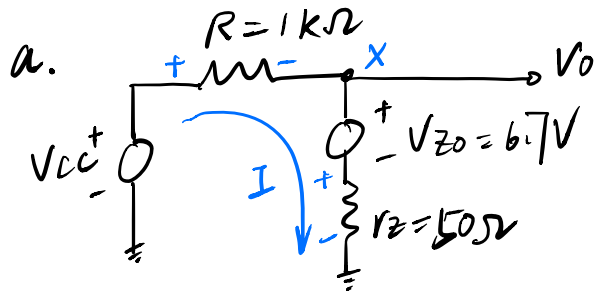
max. allowed resistance:

$$r_d = 0.2024 \Omega$$

$$10 \times 10^{-3} V = 1V \cdot \frac{\left(\frac{1}{100} + \frac{1}{r_d} \right)^{-1}}{\left(\frac{1}{100} + \frac{1}{r_d} \right)^{-1} + 20}$$

3

Problem (3)



KVL: $(R + r_z) \cdot I = V_{CC} - V_{Z0}$

$I = \frac{15 - 6.7}{1000 + 50} = 7.905 \text{ mA}$

$V_o = V_{Z0} + r_z \cdot I$
 $= 6.7 + 50 \times 7.905 \text{ mA}$

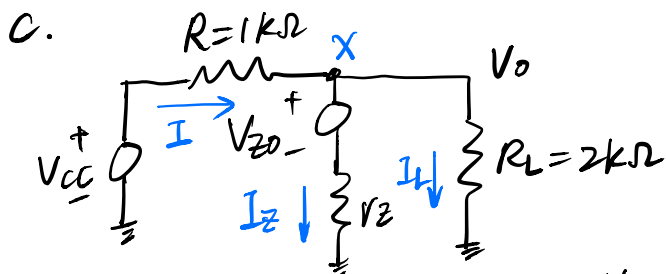
$V_o = 7.095 \text{ V}$

b. $V_{\text{ripple}} = \pm 1 \text{ V}$

$\frac{\Delta V_o}{V_{\text{ripple}}} = \frac{r_z}{R + r_z} = \frac{50}{1050}$

$\Delta V_o = \frac{50}{1050} \times (\pm 1 \text{ V}) = \pm 47.619 \text{ mV}$

$\Delta V_o = \pm 47.619 \text{ mV}$



KCL at node X:

$I = I_{Zk} + I_L$

$\frac{15 - V_o}{1000} = \frac{V_o - 6.7}{50} + \frac{V_o}{2000}$

$$\begin{cases} I = \frac{V_{CC} - V_o}{R} \\ I_Z = \frac{V_o - V_{Z0}}{r_z} \\ I_L = \frac{V_o}{R_L} \end{cases}$$

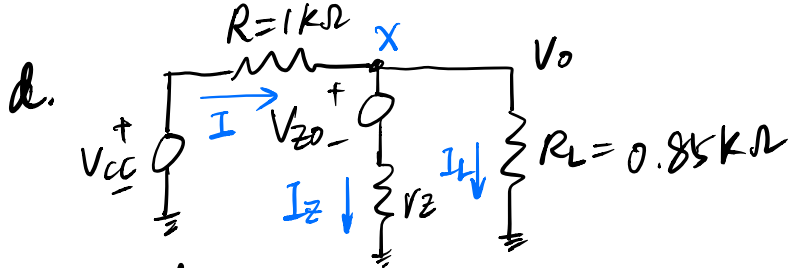
$V_o = 6.93 \text{ V}$

change in V_o (compared to "No load" case in part a)

$\Delta V_o = 6.93 \text{ V} - 7.095 \text{ V} = -0.165 \text{ V}$

checks: $I_Z = \frac{V_o - V_{Z0}}{r_z} = \frac{6.93 \text{ V} - 6.7 \text{ V}}{50 \Omega} = 4.6 \text{ mA} > I_{Zk} = 0.5 \text{ mA} \rightarrow$ The Zener is in breakdown region.

4



KCL at node x:

$$I = I_{zk} + I_L$$

$$\begin{cases} I = \frac{V_{cc} - V_o}{R} \\ I_z = \frac{V_o - V_{zo}}{r_z} \\ I_L = \frac{V_o}{R_L} \end{cases}$$

$$\frac{15 - V_o}{1000} = \frac{V_o - 6.7}{50} + \frac{V_o}{850}$$

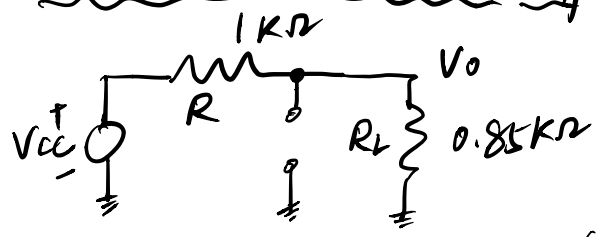
$$V_o = 6.719V$$

checks

$$I_z = \frac{V_o - V_{zo}}{r_z} = 0.38 \text{ mA} < I_{zk} = 0.5 \text{ mA}$$

"doesn't satisfy the breakdown region condition"

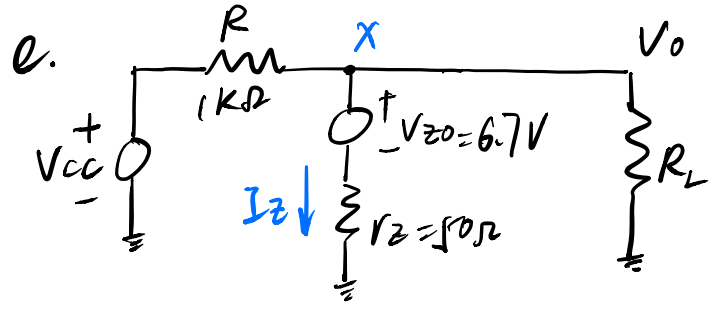
Assume the diode is "off":



$$V_o = V_{cc} \cdot \frac{R_L}{R + R_L} = 6.892V$$

change in V_o (compared to "No load" case in part c)

$$\Delta V_o = 6.892V - 7.095V = -0.203V$$



$$14V < V_{cc} < 16V$$

$$I > 0.5 \text{ mA}$$

$$V_o > V_{zo} + r_z \cdot I_z = 6.725V$$

KCL at node x:

$$(V_{cc} - V_o) \frac{1}{R} = I_z + \frac{V_o}{R_L}$$

$$R_L = \frac{V_o}{\frac{V_{cc} - V_o}{R} - I_z}$$

5

$$V_{CC} = 14V, R_L > \frac{6.725}{\frac{14-6.725}{1000} - 0.5 \times 10^{-3}} = 992.62 \Omega$$

$$V_{CC} = 16V, R_L > \frac{6.725}{\frac{16-6.725}{1000} - 0.5 \times 10^{-3}} = 766.38 \Omega$$

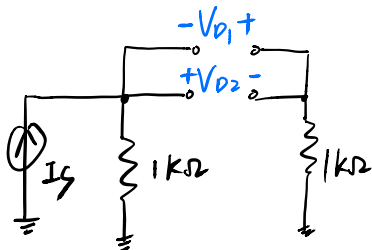
$$R_L(\min) = 992.62 \Omega$$

ensures $I_Z > 0.5 \text{ mA} = I_{ZK}$
within the complete range of V_{CC} .

6

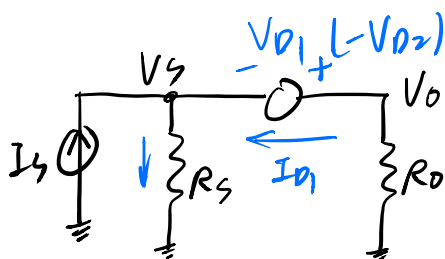
Problem (4)

① when $-0.7\text{mA} < I_S < 0.7\text{mA}$, both diodes are off, no currents flowing through R_0 , $V_0 = 0$



(checks) $|V_{D1}| = |V_{D2}| = |V_0 - V_S| = |I_S \cdot 1\text{k}\Omega| < 0.7\text{V}$, both diodes are off

② when $I_S < -0.7\text{mA}$, D_1 is on, D_2 is off.



$$V_S = V_0 - 0.7$$

$$I_S = \frac{V_S}{R_S} + \frac{V_0}{R_0} = \frac{2V_0 - 0.7}{1\text{k}\Omega}$$

$$2V_0 - 0.7 = I_S \times 1\text{k}\Omega$$

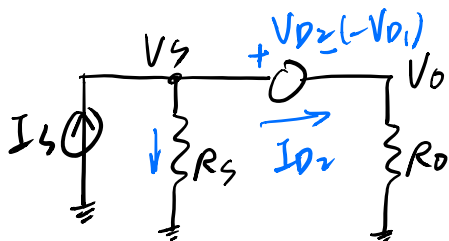
with $I_S = -2\text{mA}$,

$$V_0 = \frac{-1.3\text{V}}{2} = -0.65\text{V}$$

(checks) $V_{D2} = V_S - V_0 = -0.7\text{V} < 0.7\text{V}$, D_2 is off

$I_{D1} = \frac{V_S}{R_S} - I_S > -0.7\text{mA} + 0.7\text{mA} = 0$, D_1 is on.

③ when $I_S > 0.7\text{mA}$, D_1 is off, D_2 is on.



$$V_S = V_0 + 0.7$$

$$I_S = \frac{V_S}{R_S} + \frac{V_0}{R_0} = \frac{2V_0 + 0.7}{1\text{k}\Omega}$$

$$2V_0 + 0.7 = I_S \times 1\text{k}\Omega$$

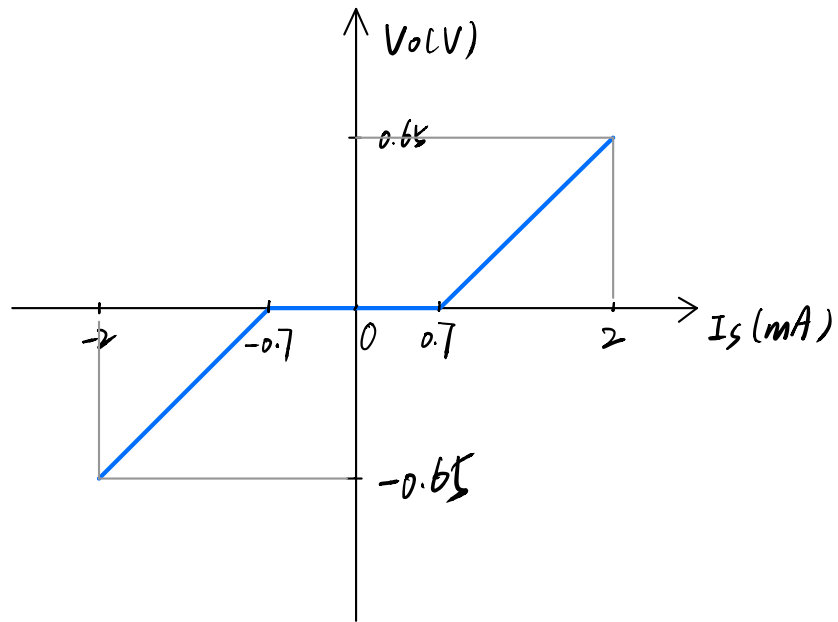
with $I_S = 2\text{mA}$,

$$V_0 = \frac{1.3}{2} = 0.65\text{V}$$

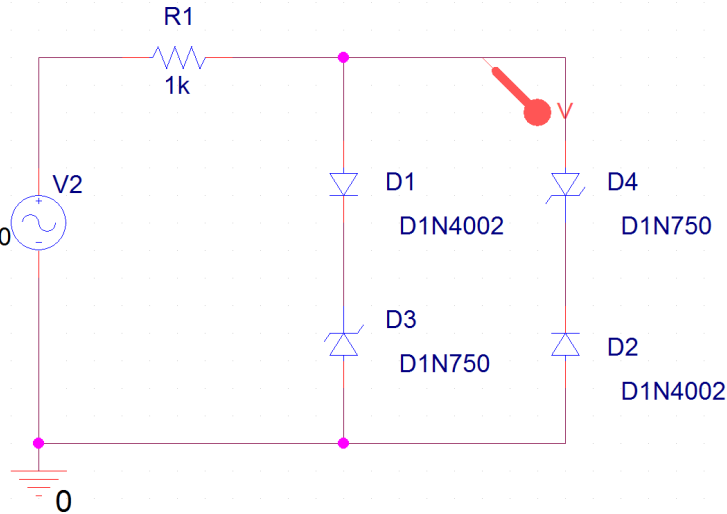
(checks) $V_{D1} = V_0 - V_S = -0.7\text{V} < 0$, D_1 is off

$I_{D2} = I_S - \frac{V_S}{R_S} > 0.7\text{mA} - 0.7\text{mA} = 0$, D_2 is on

①

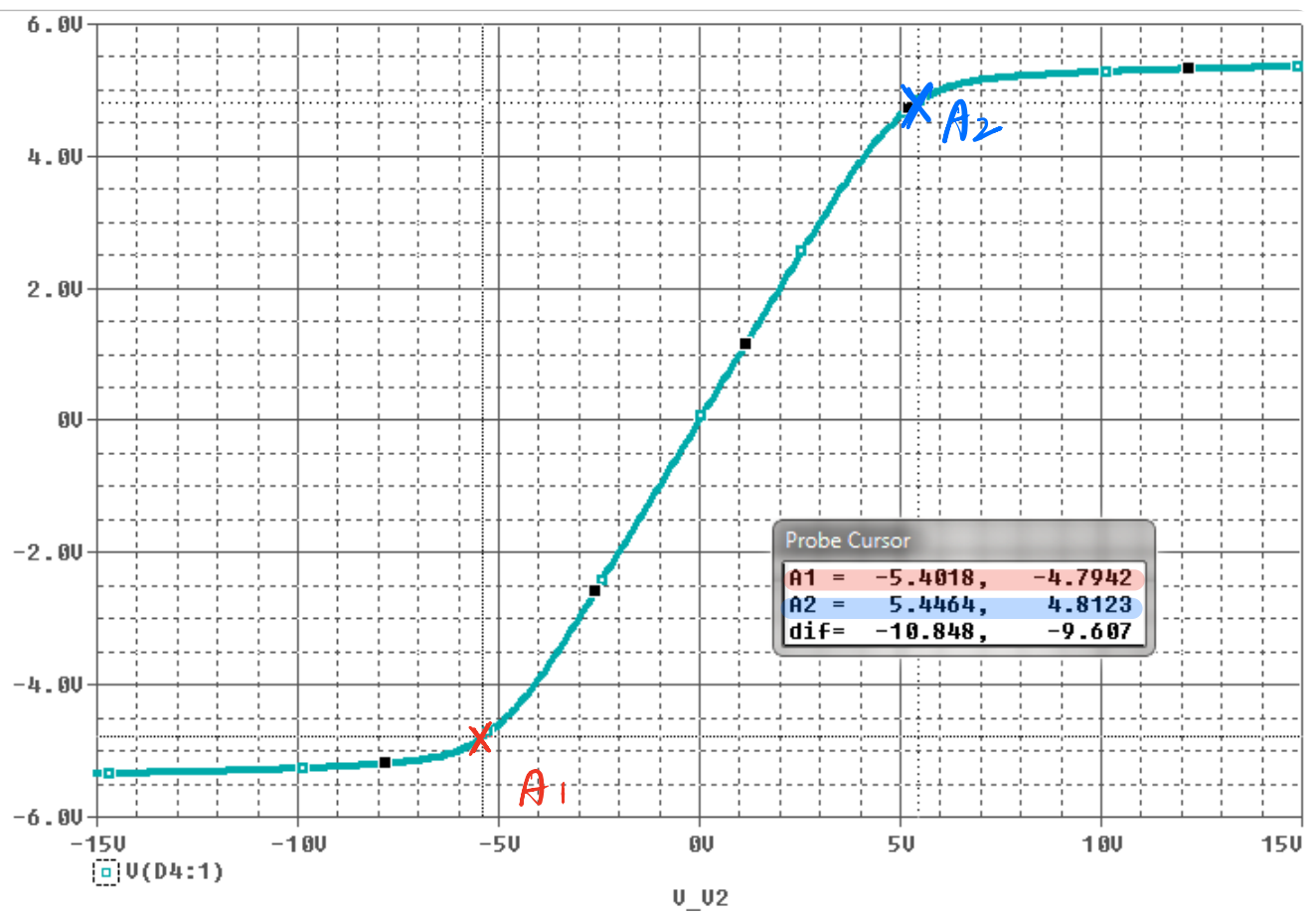


8 Problem (b)

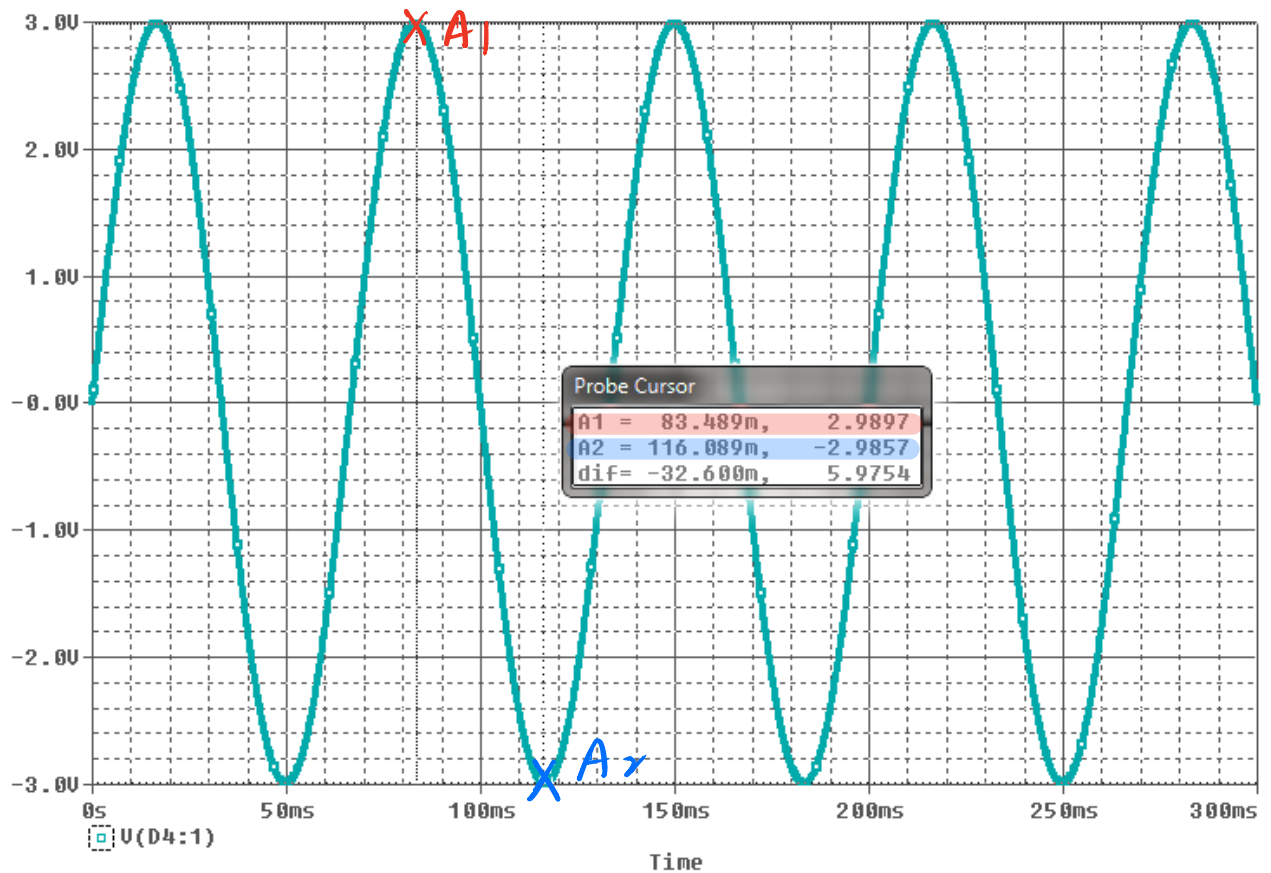


$\omega = 30\pi$
 $f = \frac{\omega}{2\pi} = 15\text{ Hz}$

DC sweeping



⑨ transient simulation ($V_{in} = 3 \sin(30\pi t)$)



transient simulation ($V_{in} = 12 \sin(30\pi t)$)

