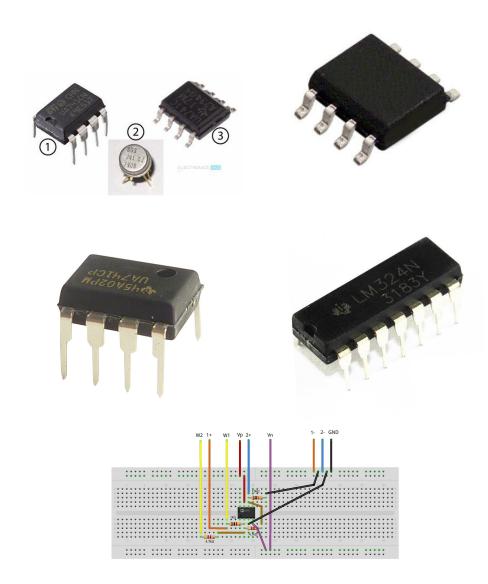
Electrical Engineering Week 5

Charles A. DiMarzio EECE–2210 Northeastern University

Sep 2022

Week 5 Agenda: Operational Amplifiers

- Amplifiers
- The Basic Op Amp
- Circuit Equations
- Virtual Short,
 - Virtual Ground
- Negative Feedback
- Inverting Amplifier
- High Gain Amplifier
- Summing Junction
- Postive Feedback Briefly
- Non-Inverting Amplifier
- Other Amplifiers



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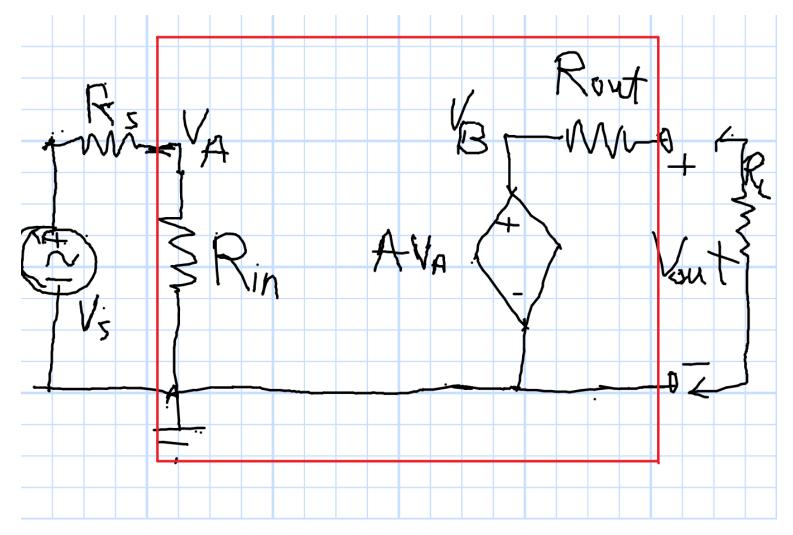
Why?

- Why Amplifiers?
 - Increase Voltage
 - Increase Current
 - Control Impedance
- Why Now?
 - Prepare for Lab
 - Nice Fit with Equivalent Circuits
- Back to Capcitors and Inductors in 2 Weeks

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An Amplifier Model

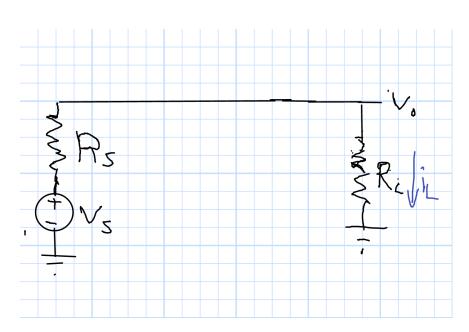


We want to Choose A, R_{in} , and R_{out}

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Impedance Choices



Voltage Divider Maximum Voltage to Load

 $R_L \gg R_s$

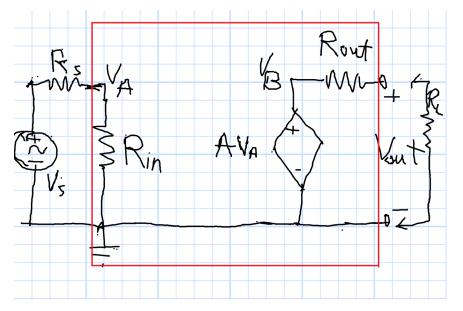
$$R_L \to \infty \text{ or } R_s \to 0$$

Maximum Power to Load

$$i_L = i = \frac{v_s}{R_s + R_L}$$
$$v_L = v_s \frac{R_L}{R_s + R_L}$$
$$p_L = v_s^2 \frac{R_L}{(R_s + R_L)^2}$$

$$R_L = R_s \qquad P_L = \frac{v_s^2}{4R_L}$$

Input and Output Impedance



Maximum Voltage

$$R_{in} \to \infty$$

 $R_{out} = 0$

Maximum Power

 $R_{in} = R_S$

 $R_{out} = R_L$

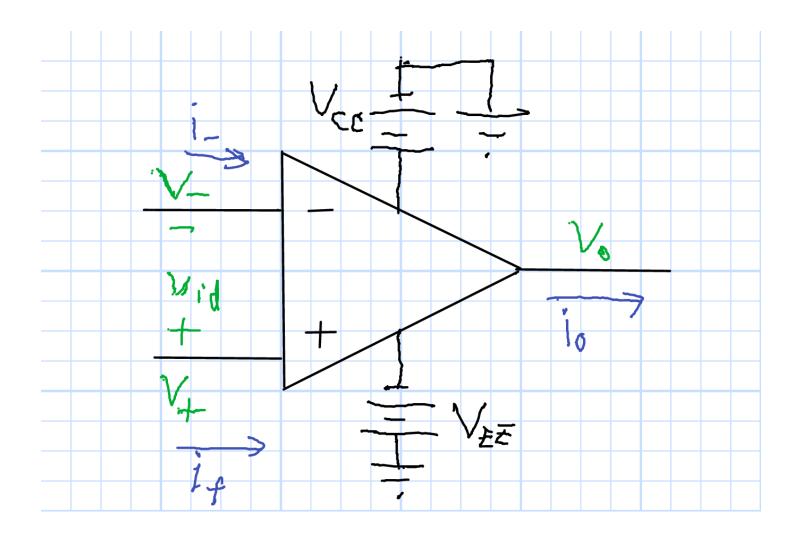
- Mix Input and Output Choices as Needed
- Maximum Power to Load for Minimum Reflected Power

Maximum Current

 $R_{in} = 0$

$$R_{out} \to \infty$$

The Operational Amplifier

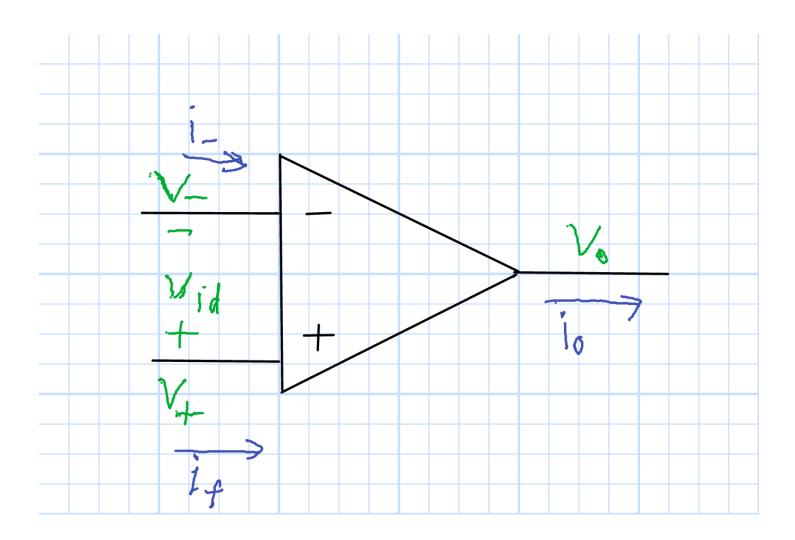


 $i_{+} = 0$ $i_{-} = 0$ $v_{o} = Av_{id}$ $A \to \infty$ "Common Mode" $((v_+ + v_-)/2)$ Gain is Zero.

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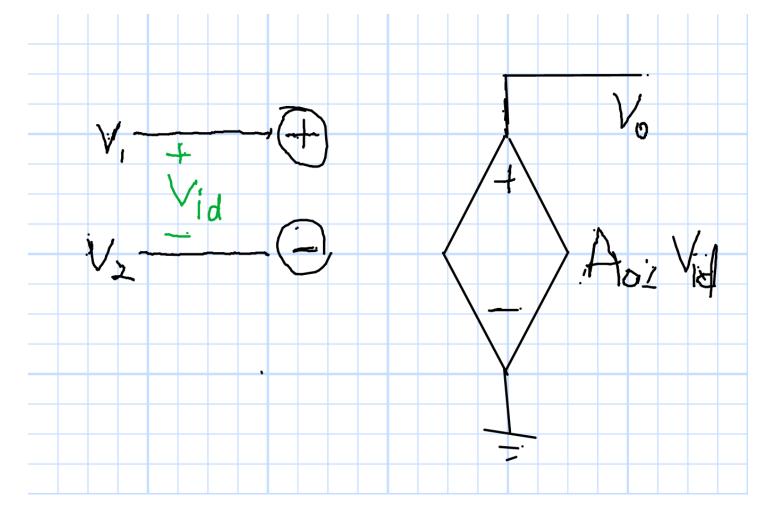
Implied Power Supplies



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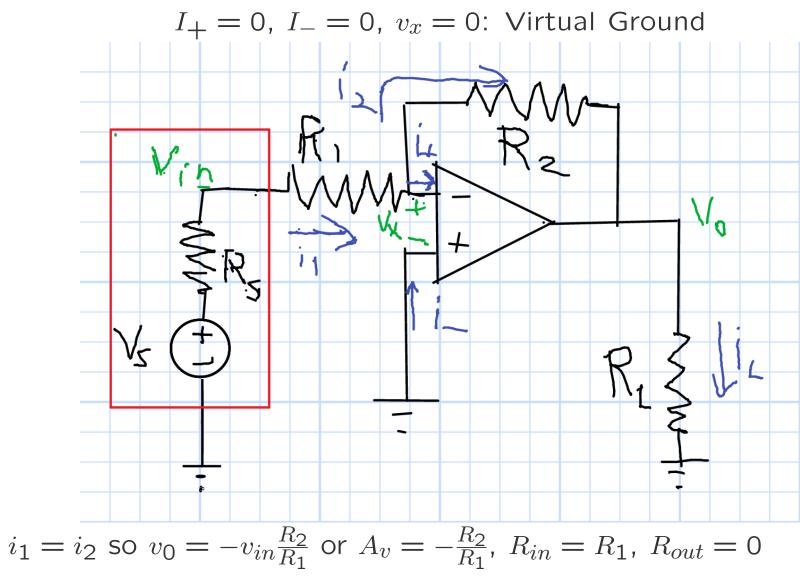
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Ideal Op-Amp Model



 $vo = A_{OL}v_{id}$ and $A_{OL} \rightarrow \infty$ so $v_{id} = 0$. Note open-circuit inputs.

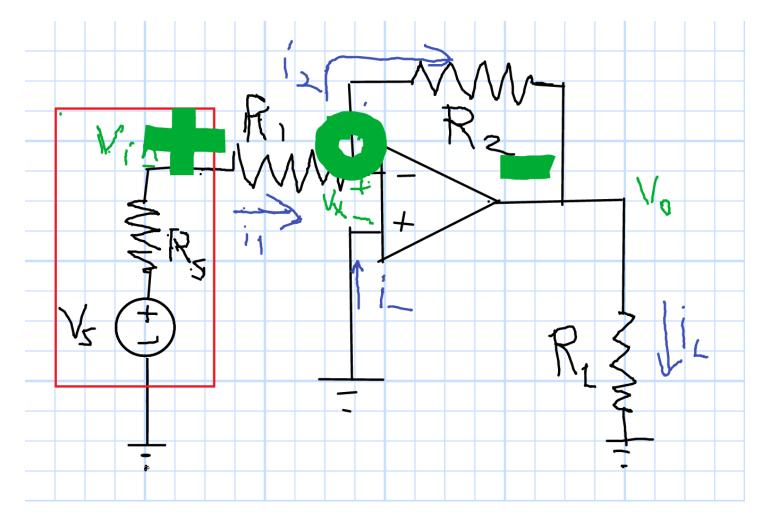
Inverting Amplifier Circuit



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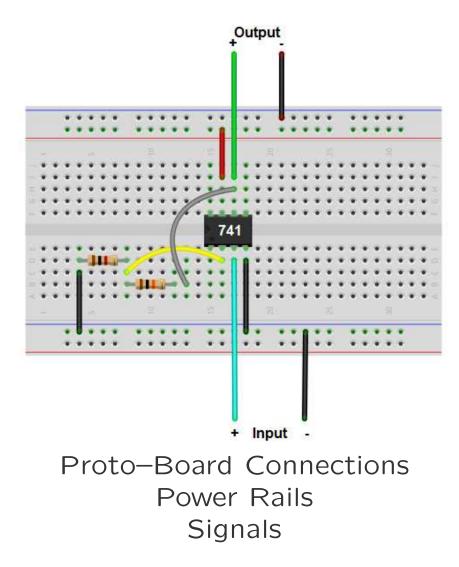
Negative Feedback

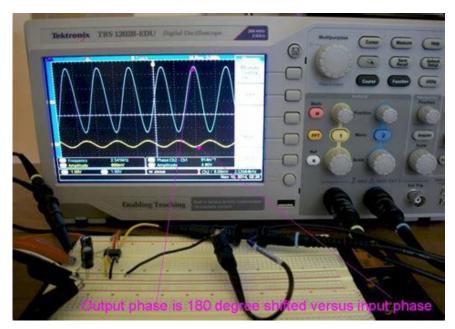


if $v_{in} > 0$, then $v_o < 0$, so v_- can be zero. if $v_{in} < 0$, then $v_o > 0$, so v_- can be zero.

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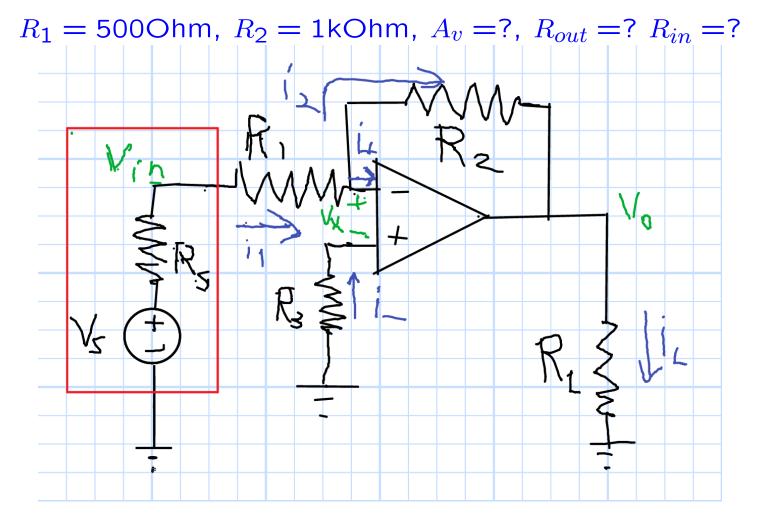
Inverting Amplifier in Lab





Measure Voltage (P-P) Frequency or Period Phase (Now 0 or 180 Deg.)

Inverting Amp Circuit?

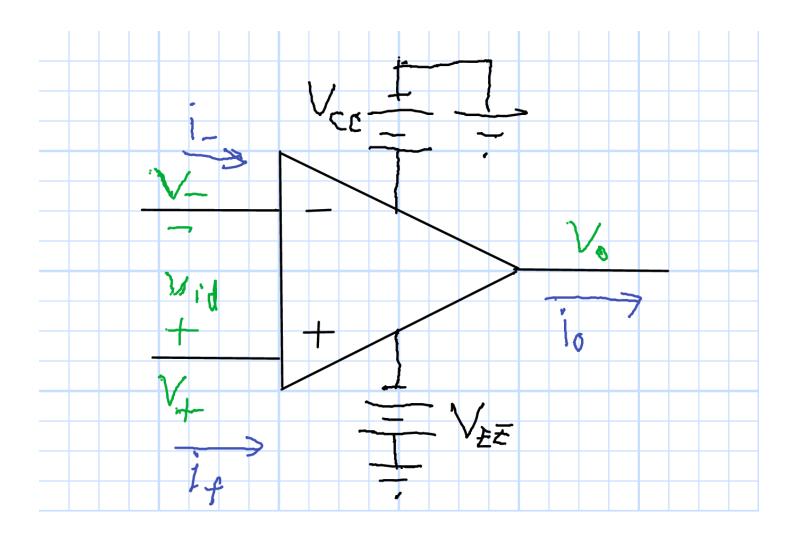


Hint: What is i_+ in R_3 ? What is v_+ ? A virtual short circuit is different from a real one.

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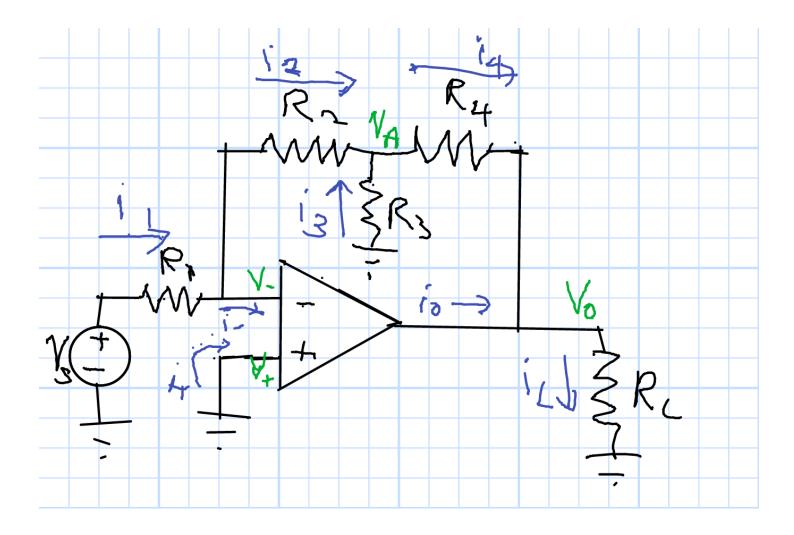
Limits on v_o



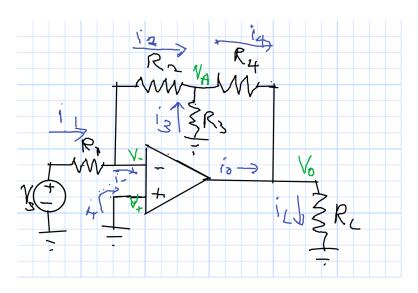
 $-V_{EE} \le v_o \le V_{CC}$

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High Gain (1)



High Gain (2)



$$i_1 = \frac{v_s}{R_1} \qquad i_2 = i_1$$

Current Divider,

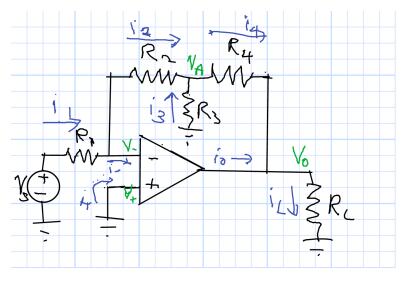
Virtual and Real Grounds

$$i_2 = i_4 \frac{R_3}{R_3 + R_2}$$

Series and Parallel Combinations

$$v_{o} = -i_{4} \left[R_{4} + (R_{2} \parallel R_{3}) \right]$$
$$v_{o} = i_{2} \frac{R_{3} + R_{2}}{R_{3}} \left[R_{4} + \frac{R_{2}R_{3}}{R_{2} + R_{3}} \right] = \frac{v_{in}}{R_{1}} \frac{R_{3} + R_{2}}{R_{3}} \left[R_{4} + \frac{R_{2}R_{3}}{R_{2} + R_{3}} \right]$$
$$= v_{in} \frac{R_{4}R_{3} + R_{4}R_{2} + R_{2}R_{3}}{R_{1}R_{3}} = v_{in} \left[\frac{R_{4}}{R_{1}} + \frac{R_{2}}{R_{1}} + \frac{R_{2}R_{4}}{R_{1}R_{3}} \right]$$

High Gain (3)



Example Values

$$\begin{aligned} R_1 &= R_3 = 1 \, \mathrm{k} \Omega & R_L &= R_1 & i_L = 440 i_{in} \\ R_2 &= R_4 = 20 \, \mathrm{k} \Omega & \text{Power Gain} \\ R_L &= 1 \, \mathrm{k} \Omega & v_o i_L = 440^2 v_s i_{in} = 193,600 v_s i_{in} \end{aligned}$$

 $v_o = v_{in} \left| \frac{R_4}{R_1} + \frac{R_2}{R_1} + \frac{R_2 R_4}{R_1 R_3} \right|$

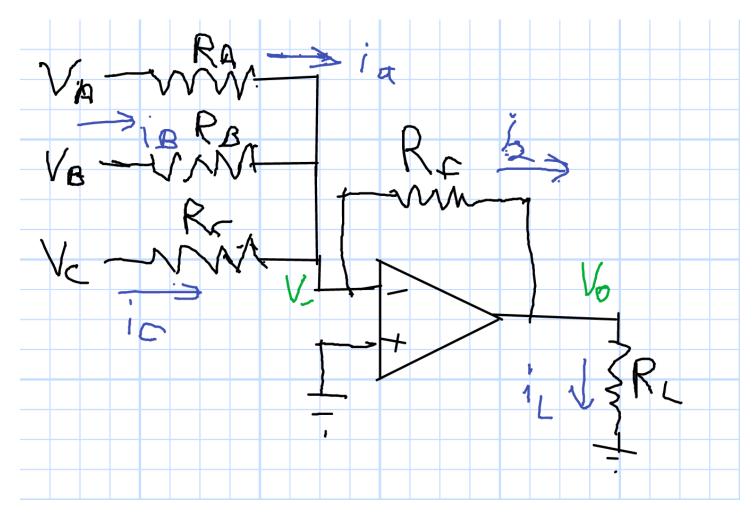
 $v_o = v_{in} (20 + +20 + 400) = 440 v_s$

 $i_{in} = i_1 = \frac{v_s}{R_1}$

 $i_L = \frac{v_o}{R_L} = 440 \frac{v_s}{R_I}$

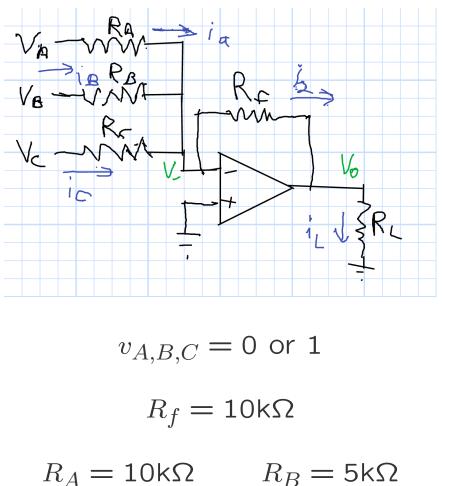
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Summing Junction



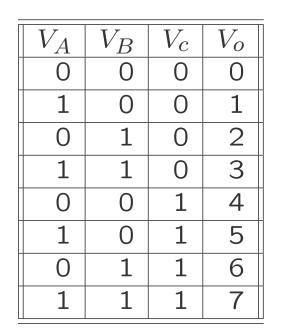
$$v_0 = -\left[\frac{R_f}{R_A}v_A + \frac{R_f}{R_B}v_B + \frac{R_f}{R_C}v_C\right]$$

Summing Junction Example

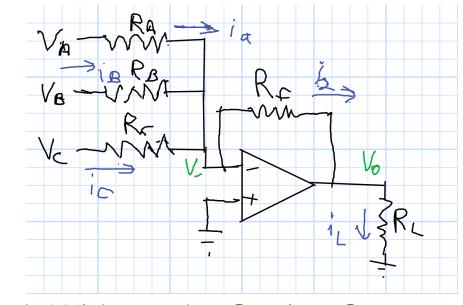


 $R_C = 2.5 \mathrm{k}\Omega$

$$v_0 = -\left[\frac{R_f}{R_A}v_A + \frac{R_f}{R_B}v_B + \frac{R_f}{R_C}v_C\right]$$

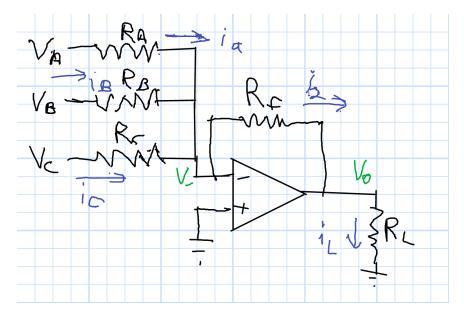


Summing Junction



Would this Work Without the Op Amp?

Summing Junction



Would this Work Without the Op Amp?

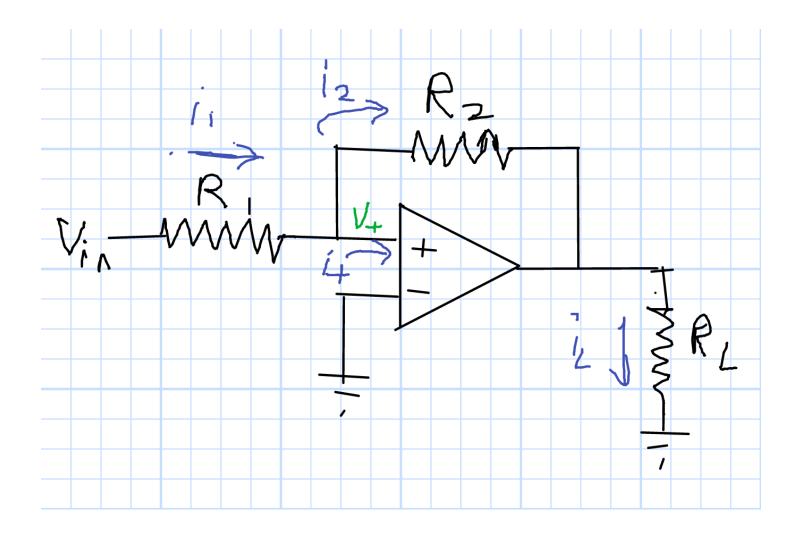
No. Connect the node v_{-} to R_{L} and remove the amplifier. Calculate the voltage at that node.

Each input circuit's voltage is affected by the other two input circuits.

The virtual ground is what makes this work.

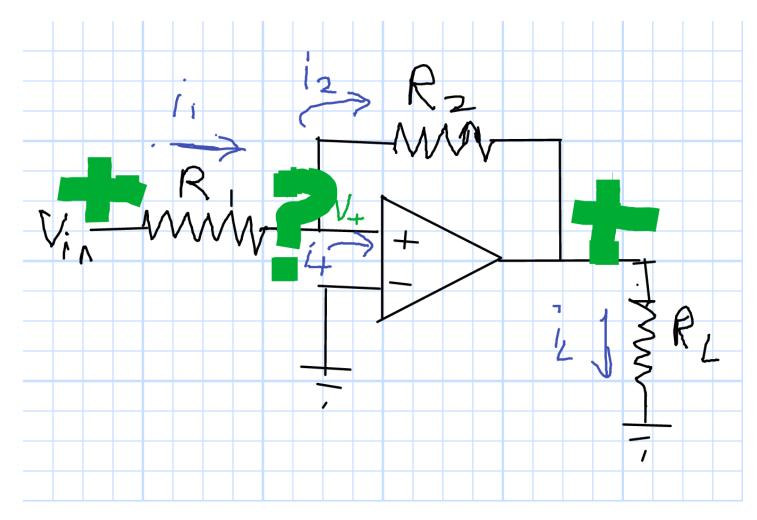
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Positive Feedback (1)



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Positive Feedback (2)

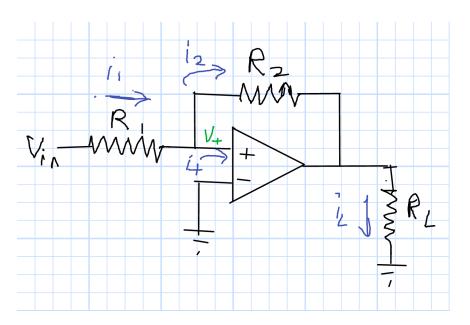


 v_0 and v_{in} have the same sign, so v_+ cannot be zero v_0 "goes to the rail." $v_0 = V_{CC}$ or $v_0 = -V_{EE}$ (actually a bit less).

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Positive Feedback (3)



 $v_{+} = v_{in} + (v_o - v_{in}) \frac{R_1}{R_1 + R_2} = v_{in} \frac{R_2}{R_1 + R_2} + v_o \frac{R_1}{R_1 + R_2}$

 v_o is limited by the power rails At what v_{in} does it switch?

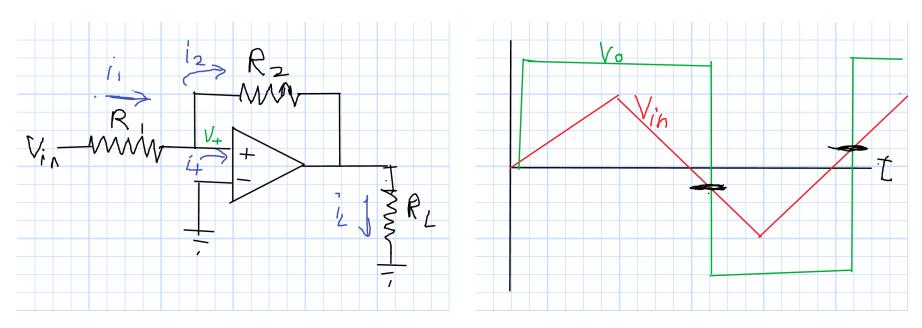
 v_{id} is not zero; Virtual ground fails. v_+ has same sign as v_o v_o "goes to the rail."

$$v_{+} = 0$$
$$v_{in} = -v_{rail} \frac{R_1}{R_2}$$

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Positive Feedback (4)



If $v_o = V_{CC}$, then it will not switch until $v_{in} < -V_{CC} \frac{R_1}{R_2}$

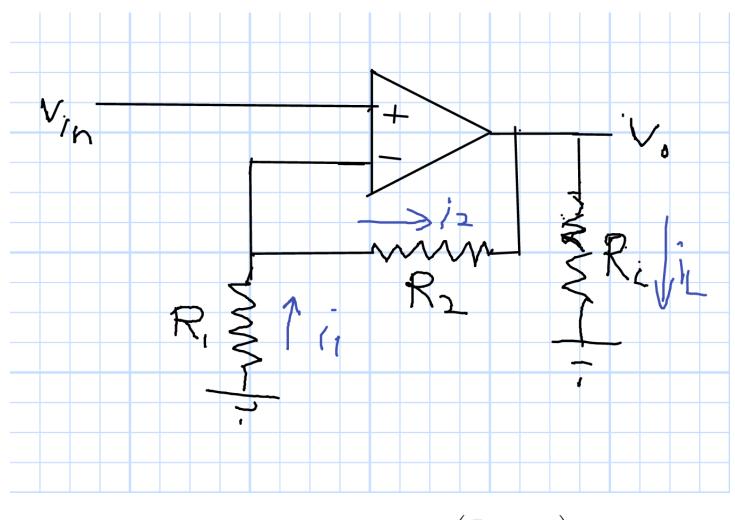
If $v_o = -V_{EE}$, then it will not switch until $v_{in} > +V_{EE}\frac{R_1}{R_2}$ The circuit is bistable.

It "remembers" how it was set until it is switched.

Normally, V_{in} could just be postive and negative pulses.

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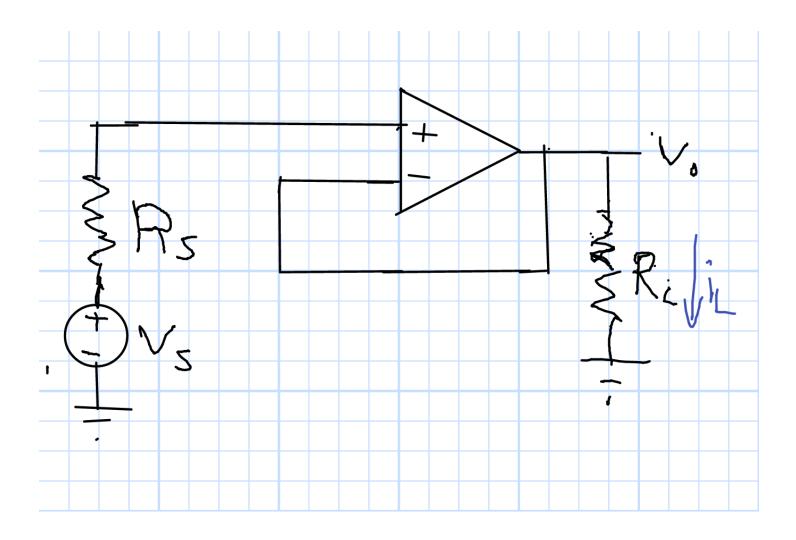
Non–Inverting Amplifier



$$v_{+} = v_{-} \qquad v_{o} = v_{in} \left(\frac{R_2}{R_1} + 1\right)$$

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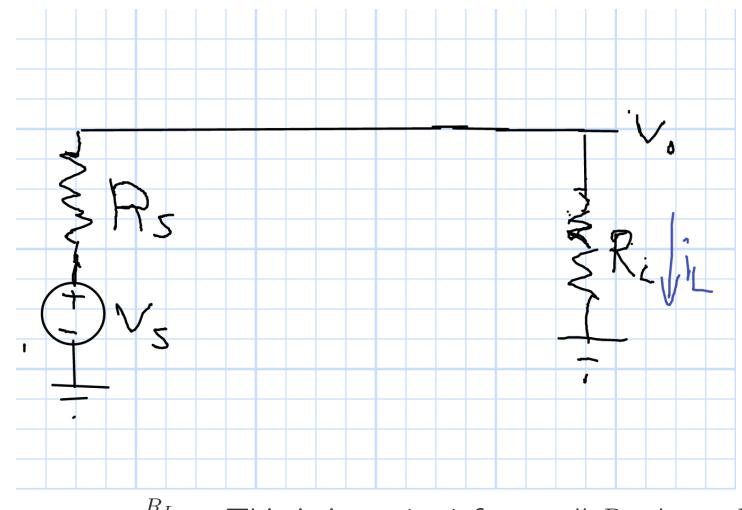
Voltage Follower



$$v_o = v_{in} = v_s \qquad i_s = 0$$

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Why Voltage Follower?

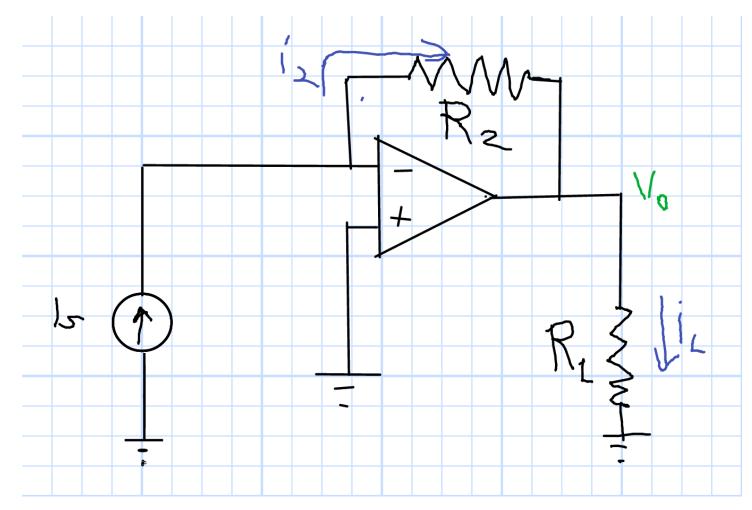


Here, $v_o = v_s \frac{R_L}{R_L + R_s}$. This is important for small R_L , large R_s . The amplifier provides the needed current.

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Transimpedance Amplifier

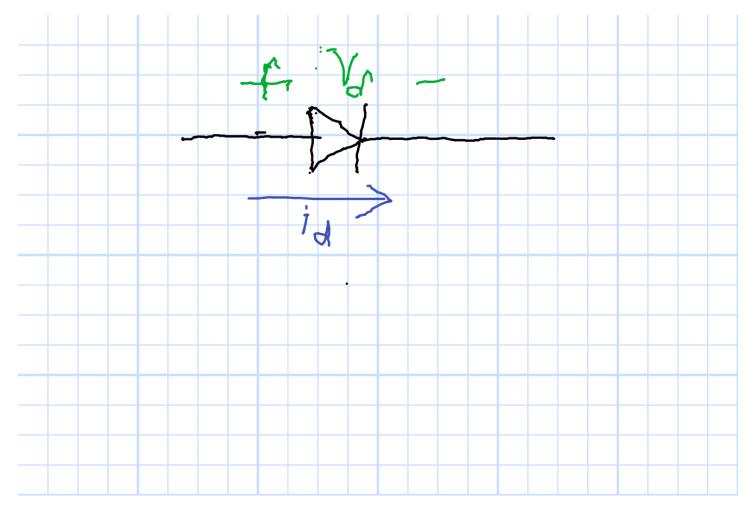


 $v_0 = -R_2 i_s$. Useful for photodiodes among other applications

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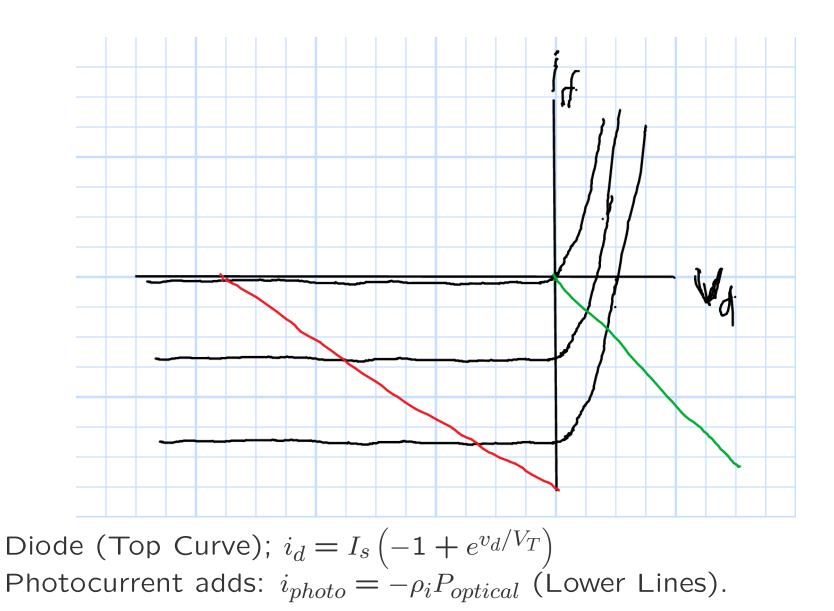
Speaking of Photodiodes...



Diode: Small reverse current & Large forward current Photodiode: Reverse current increases with optical power.

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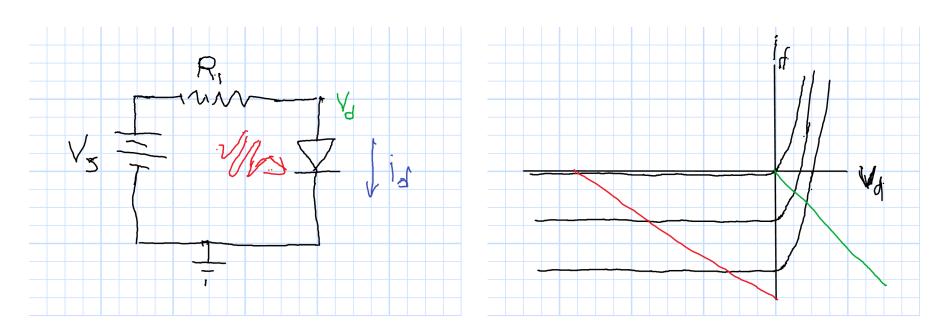
Photodiode Curves



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Photodiode Circuit



$$v_d = v_s + \rho_i P_{optical} R_1$$

Photocurrent is Negative

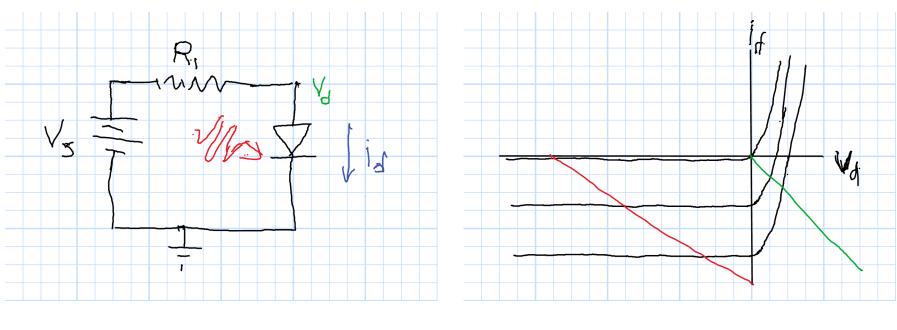
 $v_s < 0$ Red Line

Useful as a detector of light. Negative Bias also helps with speed.

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Solar Cell



 $v_s = 0$ $P_{diode} < 0$ Green Line

Diode is a source of power.

 $R_!$ is the load.

$$P_L = -P_{diode}$$